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1 **SECOND ORDER HOMOGENIZATION OF SUBWAVELENGTH**
2 **STRATIFIED MEDIA INCLUDING FINITE SIZE EFFECT**

3 JEAN-JACQUES MARIGO* AND AGNÈS MAUREL†

4 **Résumé.** We present a homogenization method to find the effective behavior of a periodically
5 stratified slab which accounts for the finite size of the slab. The effective behavior is that of a
6 homogeneous anisotropic slab associated with discontinuity conditions, or jump conditions, for the
7 displacement and for the normal stress at the boundaries of the slab. The coefficients entering in
8 the effective homogenized wave equation are related to the geometry and to the composition of the
9 layers only, as in the classical homogenization. Those entering in the jump conditions are related to
10 boundary layer effects and thus they depend also on the properties of the media surrounding the
11 slab. The validity of our homogenization method is inspected in the case of layers associated with
12 Neumann boundary conditions.

13 **Key words.** homogenization, two-scale method, matched asymptotic expansion, stratified me-
14 dia, finite size effects, effective jump conditions,

15 **AMS subject classifications.** 34E13, 35B27,74Q10, 74Q15,80M35, 74J20,

16 **1. Introduction.** The scattering properties of media stratified at a subwave-
17 length scale are known to be correctly described by an equivalent homogeneous aniso-
18 tropic medium whose effective bulk parameters involve averages of the bulk paramete-
19 rs of the layers (the parameters entering in the wave equations); for shear horizontal
20 (SH) elastic waves, it is the mass density and the shear modulus, and the averages
21 involve also the surface or volume fractions of the layers. This is known since Rytov’s
22 work in 1956 [14] and the result has been extended within a rigorous mathematical
23 framework to periodic media using the homogenization theory, see *e.g.* [3].

24 In its classical form, the homogenization is performed considering that the structu-
25 red medium occupies the whole space. Obviously in practice, samples of finite thickness
26 e are considered and it has been shown that, for small e , the scattering properties of
27 the samples were not correctly described by their homogenized counterparts [7, 8, 9].
28 In this paper, we show that the homogenization theory can be adapted to stratified
29 structures of finite thickness, which yields an equivalent slab whose scattering proper-
30 ties accurately describe those of the actual structure. We establish that, in addition
31 to the bulk parameters entering in the effective wave equation, the homogenization
32 makes interface parameters to appear, which enter in jump conditions at the bound-
33 aries of the equivalent slab (Figure 1). While the effective bulk parameters depend
34 only on the characteristics of the structure at the microscale, the interface parameters
35 result from boundary layer effects and as such, they depend also on the characteristics
36 of the surrounding media.

37 The homogenization for finite size stratified structures is performed up to the
38 second order in $\varepsilon \equiv kh \ll 1$ (k being the wavelength and h the periodicity of the
39 structure). It is presented in the section 2 and the approach essentially follows the
40 one presented in [1] in the context of solid mechanics. We start with the elastic wave
41 equation for the scalar displacement field $U(\mathbf{X})$ of shear waves written in the harmonic
42 regime

43 (1) $\operatorname{div}(\mu \nabla U) + \rho \omega^2 U = 0,$

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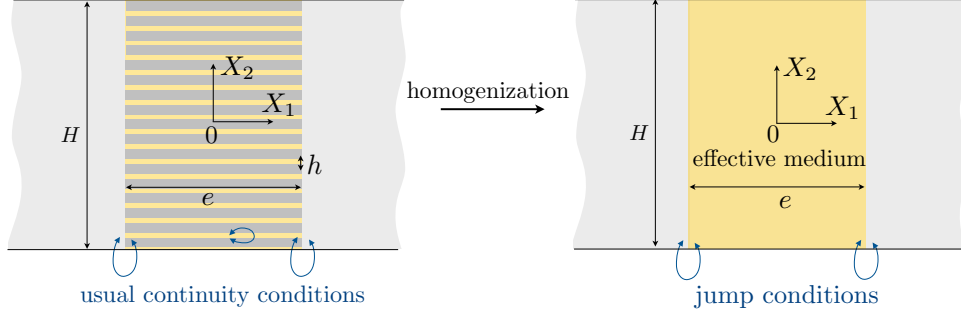


FIGURE 1. On the left, the wave problem is set for a slab filled with a stratified medium, with the usual continuity conditions on the boundaries of the layers. On the right, it is set for an equivalent slab made of an effective medium (homogeneous and anisotropic) and jump conditions apply at the boundaries of the slab $X_1 = \pm e/2$ (the boundaries at $|X_2| = H/2$ are disregarded or equivalently, we consider $H \rightarrow +\infty$).

with $\mu(\mathbf{X})$ the shear modulus and $\rho(\mathbf{X})$ the mass density being spatially dependent of $\mathbf{X} = (X_1, X_2) \in \mathbb{R} \times (-H/2, H/2)$ and ω the frequency (Fig. 1). Eq. (1) can be written using the non dimensional parameters

$$\alpha(\mathbf{X}) \equiv \frac{\mu(\mathbf{X})}{\mu_m}, \quad \text{and} \quad \beta(\mathbf{X}) \equiv \frac{\rho(\mathbf{X})}{\rho_m},$$

44 with (μ_m, ρ_m) the shear modulus and mass density of the medium surrounding the
 45 stratified structure, hereafter called the substrate; with $k = \omega \sqrt{\rho_m/\mu_m}$ the wavenum-
 46 ber in the substrate, we get

$$47 \quad (2) \quad \operatorname{div}(\alpha \nabla U) + \beta k^2 U = 0,$$

48 which also applies to acoustic waves, to transverse magnetic or transverse electric
 49 polarized electromagnetic waves or to scalar (shear) elastic waves. It follows that the
 50 Helmholtz equation $\Delta U + k^2 U = 0$ applies in the substrate by construction. We shall
 51 establish that the homogenized wave equation, up to second order, is of the form

$$52 \quad (3) \quad \operatorname{div} \Sigma + \beta^{\text{eff}} k^2 U = 0, \quad \Sigma = \begin{pmatrix} \alpha_1^{\text{eff}} & 0 \\ 0 & \alpha_2^{\text{eff}} \end{pmatrix} \nabla U,$$

53 where $(\alpha_1^{\text{eff}}, \alpha_2^{\text{eff}}, \beta^{\text{eff}})$ will be defined in subsection 2.2, see (27). Next, for the stratified
 54 medium occupying the region $\mathbf{X} = (X_1, X_2) \in (-e/2, e/2) \times (-H/2, H/2)$, the homo-
 55 genized slab, in which (3) applies, occupies the same region and effective continuity
 56 or discontinuity conditions apply at $X_1 = \pm e/2$. While the usual continuities of the
 57 displacement U and of the normal stress $\Sigma \cdot \mathbf{N}$ are obtained at the first order, dis-
 58 continuities of these quantities at second order are established. Specifically, the jump
 59 conditions read

$$60 \quad (4) \quad \begin{cases} \llbracket U \rrbracket = \frac{h\mathcal{B}}{2} (\Sigma^- + \Sigma^+) \cdot \mathbf{N}, \\ \llbracket \Sigma \rrbracket \cdot \mathbf{N} = -\frac{h\mathcal{C}}{2} \left(\frac{\partial^2 U^-}{\partial X_2^2} + \frac{\partial^2 U^+}{\partial X_2^2} \right). \end{cases}$$

61 In the above relations, for any field V being discontinuous across a boundary with
 62 (V^-, V^+) its values on both sides, we have defined the jump $\llbracket V \rrbracket \equiv V^+ - V^-$ (and

63 the convention \pm refers to the direction of the normal \mathbf{N}). The parameters $(\mathcal{B}, \mathcal{C})$
 64 entering in the jump conditions are deduced from elementary problems, being the
 65 equivalent of the cell problems in the classical homogenization, Eqs. (34) and (35). In
 66 the absence of high contrasts resulting in possible resonances in one or several layers
 67 (and possible resonances are disregarded here), these problems are static problems
 68 that can be solved once and for all. Finally, the problem of the boundary layers at the
 69 boundaries $X_2 = \pm H/2$ would require a specific treatment and they are disregarded
 70 in the present paper (alternatively, we may consider $H \rightarrow +\infty$).

71 Validations of our homogenization method are presented in section 3 by compa-
 72 rison with full wave numerics. We restrict ourselves to the case of layers associated
 73 with Neumann boundary conditions; it corresponds to cracks or voids in elasticity, to
 74 sound hard inclusions in acoustics or to perfectly conducting metals in electromagne-
 75 tism. This case allows for explicit expressions of the interface parameters $(\mathcal{B}, \mathcal{C})$, Eq.
 76 (53) (see also subsection S2.1). The limitations of the present approach to small slab
 77 thicknesses are discussed in Appendix A. Finally, we report in section S1 the case of
 78 a stratified slab with one boundary being free of stresses (associated with Neumann
 79 boundary condition) and details on the numerical resolutions are given in section S2.

80 **2. Up to second-order homogenization.** In this section, we shall work on
 81 a problem simplified with respect to the one in Fig. 1 in the sense that we consider
 82 a single interface (also, we shall work in dimensionless coordinates). We define $x_1 =$
 83 $k(X_1 - e/2)$, $x_2 = kX_2$, which means that we focus on a region near the boundary
 84 of the stratified medium at $X_1 = e/2$ in the original problem in Fig. 1(a). But now,
 85 we assume that the stratified medium occupies the region $x_1 < 0$, Fig. 2. Doing
 86 so, we assumed implicitly that the wave passing through the stratified slab in the
 87 configuration of the Fig. 1 feels the boundaries and the *bulk of the stratified medium*.
 88 To anticipate, this means that the slab is thick enough, and thick means that the
 89 evanescent fields at both boundaries of the slab do not interact. If it is not the case, one
 90 should consider the whole thin slab in the asymptotic analysis, as done in [5, 6, 9, 11]
 (this is discussed further in Appendix A).

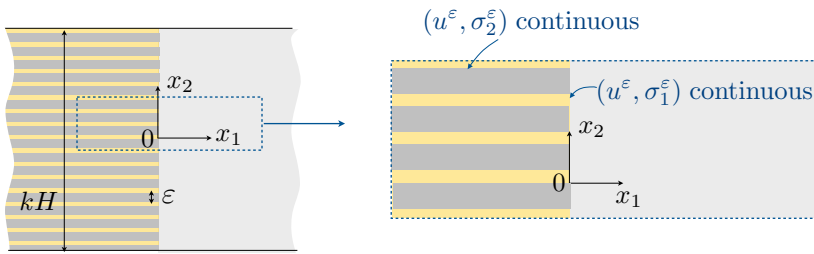


FIGURE 2. Single interface between the stratified medium occupying the region $x_1 < 0$ and the substrate occupying the region $x_1 > 0$. The usual continuity conditions apply at the boundaries between the layers $(u^\varepsilon, \sigma_2^\varepsilon)$ and at the boundaries between the layers and the substrate $(u^\varepsilon, \sigma_1^\varepsilon)$ at $x_1 = 0$.

91 We shall define the actual problem for $\mathbf{x} = (x_1, x_2) \in \mathbb{R} \times (-kH/2, kH/2)$. With
 92 the periodicity of the stratified medium $\varepsilon = kh \ll 1$, the solution of the problem
 93 depends on ε and we make this dependence to appear explicitly, by denoting $a^\varepsilon(\mathbf{x}) \equiv$
 94 $\alpha(\mathbf{X})$, $b^\varepsilon(\mathbf{x}) \equiv \beta(\mathbf{X})$ and $u^\varepsilon(\mathbf{x}) \equiv U(\mathbf{X})$, $\sigma^\varepsilon(\mathbf{x}) \equiv k^{-1}\alpha(\mathbf{X})\nabla U(\mathbf{X})$. In \mathbf{x} -coordinate,

96 (2) reads

97 (5a) $\operatorname{div} \boldsymbol{\sigma}^\varepsilon(\mathbf{x}) + b^\varepsilon(\mathbf{x})u^\varepsilon(\mathbf{x}) = 0,$

98 (5b) $\boldsymbol{\sigma}^\varepsilon(\mathbf{x}) = a^\varepsilon(\mathbf{x})\nabla u^\varepsilon(\mathbf{x}),$

100 and

101 (6) $a^\varepsilon(\mathbf{x}) = \begin{cases} 1, & x_1 > 0, \\ a\left(\frac{x_2}{\varepsilon}\right), & x_1 < 0. \end{cases} \quad b^\varepsilon(\mathbf{x}) = \begin{cases} 1, & x_1 > 0, \\ b\left(\frac{x_2}{\varepsilon}\right), & x_1 < 0. \end{cases}$

102 The functions a and b are 1-periodic and piecewise constant; at this point, it is not
 103 necessary to define them more specifically. To (5), we have to associate boundary
 104 conditions. At each boundary between two different media, the continuity of the dis-
 105 placement u^ε and of the normal stress $\boldsymbol{\sigma}^\varepsilon \cdot \mathbf{n}$ apply (with \mathbf{n} the vector normal to the
 106 boundary); this applies at the boundaries between two layers within the stratified
 107 medium and at the boundaries between the layers and the substrate at $x_1 = 0$ (Fig.
 108 2). Finally, once the wave source is defined, the conditions satisfied by $(u^\varepsilon, \boldsymbol{\sigma}^\varepsilon)$ for
 109 $x_2 = \pm kH/2$ and for $|x_1| \rightarrow +\infty$, often referred as to radiation conditions, can be
 110 defined; for the time being, we do not need to specify them.

111 **2.1. The asymptotic analysis.** The idea is to define three regions where dif-
 112 ferent asymptotic expansions will be used, Eqs. (7). The inner region contains the
 113 boundary between the stratified medium and the substrate. Roughly speaking, it is
 114 the region where the boundary layer effects are significant; in terms of wavefield, this
 115 means that the inner region contains the so-called evanescent field vanishing far from
 116 the boundary. The two outer regions for $x_1 > 0$ and $x_1 < 0$ are the regions far enough
 117 from the interface, where the evanescent field can be neglected. Next, the inner region
 118 and the outer regions are connected using so-called matching conditions, which will
 119 constitute the boundary conditions for the outer solutions.

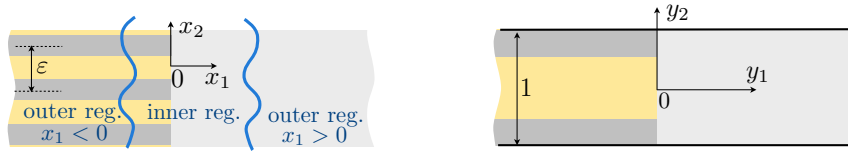


FIGURE 3. On the left, configuration in \mathbf{x} coordinate; the periodicity along x_2 is $\varepsilon \equiv kh$; the inner region corresponds to the neighborhood of the boundary between the stratified medium ($x_1 < 0$) and the substrate being a homogeneous medium ($x_1 > 0$). On the right, the unit cell (inner region) in \mathbf{y} coordinate, with $\mathbf{y} = \mathbf{x}/\varepsilon$, and $\mathbf{y} \in \mathbb{R} \times Y$, with $Y = (-1/2, 1/2)$.

120 **2.1.1. The outer and inner expansions.** As in the classical homogenization,
 121 the asymptotic expansions are thought with spatial dependences on a *macroscopic*
 122 coordinate \mathbf{x} associated with slow variations of the fields (with the typical scale $1/k$
 123 of the wave) and a *microscopic* coordinate \mathbf{y} , associated with rapid variations (the
 124 typical scale h of the layers), and in each region, we keep the coordinates that are
 125 relevant to describe the variations of the field. To do so, we define $\mathbf{y} \equiv \mathbf{x}/\varepsilon$ and we

126 assume that $(u^\varepsilon, \sigma^\varepsilon)$ can be expanded by using the following asymptotic expansions

$$127 \quad (7) \quad \left\{ \begin{array}{l} \text{outer region } x_1 > 0, \quad u^\varepsilon = u^0(\mathbf{x}) + \varepsilon u^1(\mathbf{x}) + \dots, \\ \quad \quad \quad \sigma^\varepsilon = \sigma^0(\mathbf{x}) + \varepsilon \sigma^1(\mathbf{x}) + \dots, \\ \text{outer region } x_1 < 0, \quad u^\varepsilon = u^0(\mathbf{x}, y_2) + \varepsilon u^1(\mathbf{x}, y_2) + \dots, \\ \quad \quad \quad \sigma^\varepsilon = \sigma^0(\mathbf{x}, y_2) + \varepsilon \sigma^1(\mathbf{x}, y_2) + \dots, \\ \text{inner region,} \quad \quad \quad u^\varepsilon = v^0(x_2, \mathbf{y}) + \varepsilon v^1(x_2, \mathbf{y}) + \dots, \\ \quad \quad \quad \sigma^\varepsilon = \tau^0(x_2, \mathbf{y}) + \varepsilon \tau^1(x_2, \mathbf{y}) + \dots, \end{array} \right.$$

128 with the outer terms (u^n, σ^n) for $x_1 < 0$ and the inner terms (v^n, τ^n) being Y -periodic
 129 with $Y = (-1/2, 1/2)$. Thus, we shall consider $y_2 \in Y$ and in the inner region $y_1 \in \mathbb{R}$;
 130 next, in the three regions $x_2 \in (-kH/2, kH/2)$ and in the outer regions $x_1 \in (-\infty, 0)$
 131 and $x_1 \in (0, +\infty)$ respectively.

132 The differential operator reads, in the different regions, as

$$133 \quad (8) \quad \left\{ \begin{array}{l} \text{in the outer region,} \quad \nabla \rightarrow \nabla_{\mathbf{x}}, \quad x_1 > 0, \\ \quad \quad \quad \nabla \rightarrow \nabla_{\mathbf{x}} + \frac{1}{\varepsilon} \frac{\partial}{\partial y_2} \mathbf{e}_2, \quad x_1 < 0, \\ \text{in the inner region,} \quad \nabla \rightarrow \frac{\partial}{\partial x_2} \mathbf{e}_2 + \frac{1}{\varepsilon} \nabla_{\mathbf{y}}, \end{array} \right.$$

134 where $\nabla_{\mathbf{x}}$ means gradient *w.r.t.* \mathbf{x} and $\nabla_{\mathbf{y}}$ means gradient *w.r.t.* \mathbf{y} . Let us comment
 135 the dependences in \mathbf{x} and \mathbf{y} of the fields in each region, (7). The inner solution is
 136 characterized by rapid variations of the evanescent field, and these variations are
 137 naturally described by \mathbf{y} ($|\nabla U| \sim U/h$ gives $|\nabla_{\mathbf{y}} u| \sim u$). But the inner solution
 138 contains also the propagating field associated with slow variations along x_2 , typically
 139 the phase variation along the boundary at $x_1 = 0$; this is taken into account by
 140 keeping x_2 as an additional coordinate. In the outer region $x_1 > 0$, there is no rapid
 141 variations due to the evanescent field (this latter being confined in the inner region,
 142 by definition); thus, we need only the coordinates \mathbf{x} which describe the propagating
 143 field with $|\nabla U| \sim kU$ and thus $\nabla_{\mathbf{x}} u \sim u$. The story is different for $x_1 < 0$; there,
 144 the field has still slow variations, but it also experiences rapid variations across the layers
 145 and this is accounted for by keeping the coordinate y_2 .

146 Finally, from (6), $(a^\varepsilon, b^\varepsilon)$ can be specified with in the outer regions

$$147 \quad (9) \quad \left\{ \begin{array}{l} \text{outer region } x_1 > 0, \quad a^\varepsilon(\mathbf{x}) = 1, \quad b^\varepsilon(\mathbf{x}) = 1, \\ \text{outer region } x_1 < 0, \quad a^\varepsilon(\mathbf{x}) = a\left(\frac{x_2}{\varepsilon}\right), \quad b^\varepsilon(\mathbf{x}) = b\left(\frac{x_2}{\varepsilon}\right), \end{array} \right.$$

148 and in the inner region $a^\varepsilon(\mathbf{x}) = \tilde{a}(\mathbf{x}/\varepsilon)$ and $b^\varepsilon(\mathbf{x}) = \tilde{b}(\mathbf{x}/\varepsilon)$ with

$$149 \quad (10) \quad \tilde{a}(\mathbf{y}) = \begin{cases} a(y_2), & y_1 < 0, \\ 1, & y_1 > 0, \end{cases} \quad \tilde{b}(\mathbf{y}) = \begin{cases} b(y_2), & y_1 < 0, \\ 1, & y_1 > 0, \end{cases}$$

150 with $a(y_2), b(y_2)$ 1-periodic and piecewise constant.

151 **2.1.2. The boundary conditions and the matching conditions.** The inner
 152 and outer problems have to be associated with boundary conditions or radiation
 153 conditions which ensure that the problems are well-posed. For the inner solution, the
 154 continuities of the displacement and of the normal stress apply at the boundaries
 155 between two layers within the stratified medium and at the boundaries between the
 156 layers and the substrate at $y_1 = 0$, whence

$$157 \quad (11) \quad v^n, \boldsymbol{\tau}^n \cdot \mathbf{n} \text{ are continuous everywhere, } n = 0, 1, \dots,$$

158 but the conditions at infinity are unknown *a priori*. Reversely, since the outer expan-
 159 sions hold true only far away from the interface, the outer terms satisfy the radiation
 160 condition (once defined) but they do not have to satisfy the continuity conditions at
 161 $x_1 = 0$; only the conditions of continuity of u^n and $\boldsymbol{\sigma}^n \cdot \mathbf{n}$ at the boundaries between
 162 the layers within the stratified medium apply for $x_1 < 0$ (thus, with $\mathbf{n} = \mathbf{e}_2$).

163 The missing conditions for the inner and outer terms are provided simultaneously
 164 by the matching conditions (see the discussion on alternative matching in [1]), at
 165 leading order

$$166 \quad (12a) \quad u^0(0^-, x_2, y_2) = \lim_{y_1 \rightarrow -\infty} v^0(x_2, \mathbf{y}),$$

$$167 \quad (12b) \quad u^0(0^+, x_2) = \lim_{y_1 \rightarrow +\infty} v^0(x_2, \mathbf{y}),$$

$$168 \quad (12c) \quad \boldsymbol{\sigma}^0(0^-, x_2, y_2) = \lim_{y_1 \rightarrow -\infty} \boldsymbol{\tau}^0(x_2, \mathbf{y}),$$

$$169 \quad (12d) \quad \boldsymbol{\sigma}^0(0^+, x_2) = \lim_{y_1 \rightarrow +\infty} \boldsymbol{\tau}^0(x_2, \mathbf{y}),$$

170 and at order ε

$$172 \quad (13a) \quad u^1(0^-, x_2, y_2) = \lim_{y_1 \rightarrow -\infty} \left[v^1(x_2, \mathbf{y}) - y_1 \frac{\partial u^0}{\partial x_1}(0^-, x_2, y_2) \right],$$

$$173 \quad (13b) \quad u^1(0^+, x_2) = \lim_{y_1 \rightarrow +\infty} \left[v^1(x_2, \mathbf{y}) - y_1 \frac{\partial u^0}{\partial x_1}(0^+, x_2) \right],$$

$$174 \quad (13c) \quad \boldsymbol{\sigma}^1(0^-, x_2, y_2) = \lim_{y_1 \rightarrow -\infty} \left[\boldsymbol{\tau}^1(x_2, \mathbf{y}) - y_1 \frac{\partial \boldsymbol{\sigma}^0}{\partial x_1}(0^-, x_2, y_2) \right],$$

$$175 \quad (13d) \quad \boldsymbol{\sigma}^1(0^+, x_2) = \lim_{y_1 \rightarrow +\infty} \left[\boldsymbol{\tau}^1(x_2, \mathbf{y}) - y_1 \frac{\partial \boldsymbol{\sigma}^0}{\partial x_1}(0^+, x_2) \right].$$

177 At order ε , the conditions are obtained using the Taylor expansions of $(u^0, \boldsymbol{\sigma}^0)$, for
 178 instance for $x_1 > 0$, $u^0(\mathbf{x}) = u^0(0^+, x_2) + x_1 \partial_{x_1} u^0(0^+, x_2) + \dots = u^0(0^+, x_2) +$
 179 $\varepsilon y_1 \partial_{x_1} u^0(0^+, x_2) + \dots$

180 **2.2. The homogenized wave equation.** We want to establish the wave equa-
 181 tion, up to second-order, satisfied by the mean fields $(\bar{u}(\mathbf{x}), \bar{\boldsymbol{\sigma}}(\mathbf{x}))$ with

$$182 \quad (14) \quad \bar{u} \equiv \langle u^0 \rangle + \varepsilon \langle u^1 \rangle, \quad \bar{\boldsymbol{\sigma}} \equiv \langle \boldsymbol{\sigma}^0 \rangle + \varepsilon \langle \boldsymbol{\sigma}^1 \rangle.$$

183 We have defined the average over $y_2 \in Y$ for any function f

$$184 \quad (15) \quad \langle f \rangle(\mathbf{x}) \equiv \int_Y dy_2 f(\mathbf{x}, y_2),$$

185 and obviously, if f does not depend on y_2 , $\langle f \rangle = f$.

186 The homogenized wave equation is sought for $x_1 < 0$ only. For $x_1 > 0$, from (5)
187 along with (9), the wave equation is

$$188 \quad (16) \quad \operatorname{div}_{\mathbf{x}} \boldsymbol{\sigma}^n + u^n = 0, \quad \boldsymbol{\sigma}^n = \nabla_{\mathbf{x}} u^n, \quad (n = 0, 1), \quad \text{for } x_1 > 0,$$

189 being the same at each order, and the fields being independent of y_2 equal their
190 averages.

191 **2.2.1. The homogenized wave equation in $x_1 < 0$ at first order.** For
192 $x_1 < 0$, the Eqs. (5), at leading order ($1/\varepsilon$), read $\partial_{y_2} \sigma_2^0 = 0 = \partial_{y_2} u^0$, whence we can
193 note

$$194 \quad (17) \quad u^0(\mathbf{x}, y_2) = u^0(\mathbf{x}), \quad \sigma_2^0(\mathbf{x}, y_2) = \sigma_2^0(\mathbf{x}),$$

195 and u^0, σ_2^0 equal their averages. Now, we establish the relation between $\langle \boldsymbol{\sigma}^0 \rangle$ and u^0 .
196 The Eqs. (5) at order ε^0 in the outer problems $x_1 < 0$ give

$$197 \quad (18) \quad \boldsymbol{\sigma}^0(\mathbf{x}, y_2) = a(y_2) \left[\nabla_{\mathbf{x}} u^0(\mathbf{x}) + \frac{\partial u^1}{\partial y_2}(\mathbf{x}, y_2) \mathbf{e}_2 \right],$$

198 and

$$199 \quad (19) \quad \operatorname{div}_{\mathbf{x}} \boldsymbol{\sigma}^0(\mathbf{x}, y_2) + \frac{\partial \sigma_2^1}{\partial y_2}(\mathbf{x}, y_2) + b(y_2) u^0(\mathbf{x}) = 0.$$

200 Averaging both equations, with $\boldsymbol{\sigma}^0(\mathbf{x}, y_2) = \sigma_1^0(\mathbf{x}, y_2) \mathbf{e}_1 + \sigma_2^0(\mathbf{x}, y_2) \mathbf{e}_2$, and owing to the
201 periodicity of u^1 and of σ_2^1 w.r.t. y_2 (thus, $\langle \partial_{y_2} u^1 \rangle = 0 = \langle \partial_{y_2} \sigma_2^1 \rangle$), we easily get the
202 wave equation at the first order

$$203 \quad (20a) \quad \langle \boldsymbol{\sigma}^0 \rangle(\mathbf{x}) = \langle a \rangle \frac{\partial u^0}{\partial x_1}(\mathbf{x}) \mathbf{e}_1 + \langle 1/a \rangle^{-1} \frac{\partial u^0}{\partial x_2}(\mathbf{x}) \mathbf{e}_2,$$

$$204 \quad (20b) \quad \operatorname{div}_{\mathbf{x}} \langle \boldsymbol{\sigma}^0 \rangle + \langle b \rangle u^0 = 0.$$

206 **2.2.2. Second-order - useful relations.** Before going to the next order, we
207 shall establish the relations (22) for u^1 and (24) for σ_2^1 , that we shall use later. Both
208 relations use the same property : consider a piecewise differentiable function $g(y)$, with
209 $g'(y)$ even ; then $(g - \langle g \rangle)$ is odd and, for any function $f(y)$ being even, $f(g - \langle g \rangle)$ is
210 odd. Thus, the integral over $y \in Y$ vanishes, from which $\langle fg \rangle = \langle f \rangle \langle g \rangle$.

211 First, from (18), we have

$$212 \quad (21) \quad \frac{\partial u^1}{\partial y_2}(\mathbf{x}, y_2) = \frac{1/a(y_2) - \langle 1/a \rangle}{\langle 1/a \rangle} \frac{\partial u^0}{\partial x_2}(\mathbf{x}),$$

213 and we used that $\sigma_2^0(\mathbf{x}) = \langle 1/a \rangle^{-1} \partial_{x_2} u^0(\mathbf{x})$ from (20a). Because $a(y_2)$ is even, $\partial_{y_2} u^1$
214 is even too, so the property on the average applies and

$$215 \quad (22) \quad \langle f(\cdot) u^1(\mathbf{x}, \cdot) \rangle = \langle f \rangle \langle u^1 \rangle(\mathbf{x}), \quad \text{for any even } f.$$

216 Integrating (21), we also have

$$217 \quad (23) \quad u^1(\mathbf{x}, y_2) = A(y_2) \frac{\partial u^0}{\partial x_2}(\mathbf{x}) + \langle u^1 \rangle(\mathbf{x}), \quad A(y_2) \equiv \int_{-1/2}^{y_2} dy \frac{1/a(y) - \langle 1/a \rangle}{\langle 1/a \rangle}.$$

218 In the above expression, we have used that $\langle A \rangle = 0$, by construction.

219 Next, we use that $\sigma_1^0(\mathbf{x}, y_2) = a(y_2)\partial_{x_1}u^0(\mathbf{x})$ from (18), and thus $\langle\sigma_1^0\rangle(\mathbf{x}) =$
 220 $\langle a\rangle\partial_{x_1}u^0(\mathbf{x})$. Inserting the resulting relation $\sigma_1^0(\mathbf{x}, y_2) = a(y_2)/\langle a\rangle\langle\sigma_1^0\rangle(\mathbf{x})$ in (19),
 221 we get

$$222 \quad \frac{\partial\sigma_2^1}{\partial y_2}(\mathbf{x}, y_2) = -\frac{a(y_2)}{\langle a\rangle}\frac{\partial\langle\sigma_1^0\rangle}{\partial x_1}(\mathbf{x}) - \frac{\partial\sigma_2^0}{\partial x_2}(\mathbf{x}) - b(y_2)u^0(\mathbf{x}).$$

223 (a, b) being even, $\partial_{y_2}\sigma_2^1$ is even *w.r.t.* y_2 , from which the property on the average
 224 applies and

$$225 \quad (24) \quad \langle f(\cdot)\sigma_2^1(\mathbf{x}, \cdot)\rangle = \langle f\rangle\langle\sigma_2^1\rangle(\mathbf{x}), \quad \text{for any even } f.$$

226 **2.2.3. The homogenized wave equation in $x_1 < 0$ at second-order.** Now,
 227 we shall establish the relation between $\langle u^1\rangle$ and $\langle\sigma^1\rangle$ (for $x_1 < 0$). Eq. (5b) at order
 228 ε reads

$$229 \quad \sigma^1(\mathbf{x}, y_2) = a(y_2)\left[\nabla_{\mathbf{x}}u^1(\mathbf{x}, y_2) + \frac{\partial u^2}{\partial y_2}(\mathbf{x}, y_2)\mathbf{e}_2\right].$$

230 To average the above equation, it is sufficient to use (22) and (24), with $a(y_2)$ being
 231 even. We get

$$232 \quad (25) \quad \begin{cases} \sigma_1^1(\mathbf{x}, y_2) = a(y_2)\frac{\partial u^1}{\partial x_1}(\mathbf{x}, y_2) & \rightarrow \langle\sigma_1^1\rangle(\mathbf{x}) = \langle a\rangle\frac{\partial\langle u^1\rangle}{\partial x_1}(\mathbf{x}), \\ \frac{1}{a(y_2)}\sigma_2^1(\mathbf{x}, y_2) = \frac{\partial u^1}{\partial x_2}(\mathbf{x}, y_2) + \frac{\partial u^2}{\partial y_2}(\mathbf{x}, y_2) & \rightarrow \langle 1/a\rangle\langle\sigma_2^1\rangle(\mathbf{x}) = \frac{\partial\langle u^1\rangle}{\partial x_2}(\mathbf{x}), \end{cases}$$

233 where the arrow indicates the average process. Next, (5a) at order ε reads

$$234 \quad \operatorname{div}_{\mathbf{x}}\sigma^1(\mathbf{x}, y_2) + \frac{\partial\sigma_2^2}{\partial y_2}(\mathbf{x}, y_2) + b(y_2)u^1(\mathbf{x}, y_2) = 0,$$

235 whose average leads to

$$236 \quad (26) \quad \operatorname{div}_{\mathbf{x}}\langle\sigma^1\rangle(\mathbf{x}) + \langle b\rangle\langle u^1\rangle(\mathbf{x}) = 0,$$

237 and we have used $\langle bu^1\rangle = \langle b\rangle\langle u^1\rangle$ from (22) and $\langle\partial_{y_2}\sigma_2^2\rangle = 0$ because σ_2^2 is periodic
 238 *w.r.t.* y_2 .

239 **2.2.4. Up to second-order homogenized wave equation.** It is now suffi-
 240 cient to gather (20) and (25)-(26) to get the homogenized wave equation up to second
 241 order for $(\bar{u}(\mathbf{x}), \bar{\sigma}(\mathbf{x}))$ in (14)

$$242 \quad (27) \quad \operatorname{div}\bar{\sigma} + \langle b\rangle\bar{u} = 0, \quad \bar{\sigma} = \begin{pmatrix} \langle a\rangle & 0 \\ 0 & \langle 1/a\rangle^{-1} \end{pmatrix} \nabla\bar{u}, \quad \text{for } x_1 < 0,$$

243 which coincides, when coming back to the real space, to (3).

244 **2.3. Jump conditions.** To the homogenized wave equation (27), we have to
 245 associate jump conditions at the interface $x_1 = 0$. In this section, we will show that
 246 the usual continuities of the displacement and of the normal stress are obtained at
 247 leading order, while the second order makes discontinuities of these two fields to
 248 appear. To that aim, we have to consider the inner solution and its matching with
 249 the two outer solutions. We are looking for the jumps of $(\bar{u}, \bar{\sigma}_1)$ defined in (14),

$$250 \quad (28) \quad \llbracket \bar{u} \rrbracket = \llbracket u^0 \rrbracket + \varepsilon \llbracket \langle u^1 \rangle \rrbracket, \quad \llbracket \bar{\sigma}_1 \rrbracket = \llbracket \langle \sigma_1^0 \rangle \rrbracket + \varepsilon \llbracket \langle \sigma_1^1 \rangle \rrbracket,$$

251 and their expressions in terms of \bar{u}^\pm and $\bar{\sigma}^\pm$, the values of \bar{u} and $\bar{\sigma}$ on both sides of
 252 the interface (at this stage, we have to distinguish the values on both sides, the fields
 253 being discontinuous).

254 **2.3.1. The jump conditions at the first order.** Eq. (5b) for the inner pro-
 255 blem at the leading order in $1/\varepsilon$ tells us that $\nabla_{\mathbf{y}}v^0 = 0$ from which v^0 does not depend
 256 on \mathbf{y} . From the previous section, we already know that $u^0(\mathbf{x})$ does not depend on y_2 ,
 257 from which the matching conditions, (12a) and (12b), give

$$258 \quad (29) \quad u^0(0^-, x_2) = u^0(0^+, x_2) = v^0(x_2), \quad \text{and} \quad \llbracket u^0 \rrbracket = 0.$$

Next, (5a) in the inner region gives at the leading order $\text{div}_{\mathbf{y}}\boldsymbol{\tau}^0 = 0$; by integrating
 this equation on $\mathbb{R} \times Y$, we get

$$\int_Y dy_2 \left[\tau_1^0(x_2, +\infty, y_2) - \tau_1^0(x_2, -\infty, y_2) \right] = 0,$$

259 (we have used the periodicity of $\boldsymbol{\tau}^0$ w.r.t. y_2 and the continuity of $\boldsymbol{\tau}^0 \cdot \mathbf{n}$ between the
 260 layers along y_2). From the matching conditions (12c)-(12d) integrated over Y , we get

$$261 \quad (30) \quad \langle \sigma_1^0 \rangle(0^-, x_2) = \sigma_1^0(0^+, x_2), \quad \text{and} \quad \llbracket \langle \sigma_1^0 \rangle \rrbracket = 0.$$

262 At first order, the usual continuities of the displacement and of the normal stress are
 263 obtained. To capture the effect of the boundary layers in the neighborhood of $x_1 = 0$,
 264 we have to go up to the second order.

265 **2.3.2. The elementary problems.** Before going to the second order, we need
 266 to inspect further the inner solution. There, the variations of $\tilde{a}(\mathbf{y})$ and $\tilde{b}(\mathbf{y})$ in (5)
 267 are more involved than the simple forms $a(y_2)$ and $b(y_2)$ considered until now for $x_1 < 0$,
 268 see (10). The difference between $\tilde{a}(\mathbf{y})$ and $a(y_2)$ will constitute the whole story. From
 269 (5a) at order ε^{-1} and (5b) at order ε^0 , we have

$$270 \quad (31) \quad \text{div}_{\mathbf{y}}\boldsymbol{\tau}^0 = 0, \quad \boldsymbol{\tau}^0(x_2, \mathbf{y}) = \tilde{a}(\mathbf{y}) \left[\frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2 + \nabla_{\mathbf{y}}v^1(x_2, \mathbf{y}) \right],$$

271 where we used that $\partial_{x_2}u^0(\mathbf{x})$ is continuous at $x_1 = 0$ as u^0 does from (29). The
 272 matching conditions (12c)-(12d) yield

$$273 \quad \left\{ \begin{array}{l} \boldsymbol{\tau}^0(x_2, -\infty, y_2) = \frac{a(y_2)}{\langle a \rangle} \langle \sigma_1^0 \rangle(0, x_2) \mathbf{e}_1 + \langle 1/a \rangle^{-1} \frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2 \\ \quad \quad \quad = a(y_2) \frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2 + a(y_2) \nabla_{\mathbf{y}}v^1(x_2, -\infty, y_2). \\ \boldsymbol{\tau}^0(x_2, +\infty, y_2) = \langle \sigma_1^0 \rangle(0, x_2) \mathbf{e}_1 + \frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2 \\ \quad \quad \quad = \frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2 + \nabla_{\mathbf{y}}v^1(x_2, +\infty, y_2). \end{array} \right.$$

274 For both limits above, the first line is given by the matching conditions with $\boldsymbol{\sigma}^0$
 275 expressed as a function of $\langle \sigma_1^0 \rangle$ and $\partial_{x_2}u^0$; it is obvious for $x_1 > 0$, and for $x_1 < 0$,
 276 we used (18) and (20a) (with $\sigma_2^0 = \langle \sigma_2^0 \rangle$ from (17)). The second line is given by
 277 the expression of $\boldsymbol{\tau}^0$ in (31) along with (10). It follows that the system satisfied by

278 $v^1(x_2, \mathbf{y})$ can be written

$$(32) \quad \left\{ \begin{array}{l} \operatorname{div}_{\mathbf{y}} \boldsymbol{\tau}^0 = 0, \text{ with } \boldsymbol{\tau}^0 = \tilde{a}(\mathbf{y}) \left[\frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2 + \nabla_{\mathbf{y}} v^1(x_2, \mathbf{y}) \right], \\ v^1 \text{ and } \boldsymbol{\tau}^0 \cdot \mathbf{n} \text{ continuous,} \\ \lim_{y_1 \rightarrow -\infty} \nabla_{\mathbf{y}} v^1(x_2, \mathbf{y}) = \langle a \rangle^{-1} \langle \sigma_1^0 \rangle(0, x_2) \mathbf{e}_1 + \frac{1/a(y_2) - \langle 1/a \rangle}{\langle 1/a \rangle} \frac{\partial u^0}{\partial x_2}(0, x_2) \mathbf{e}_2, \\ \lim_{y_1 \rightarrow +\infty} \nabla_{\mathbf{y}} v^1(x_2, \mathbf{y}) = \langle \sigma_1^0 \rangle(0, x_2) \mathbf{e}_1, \end{array} \right.$$

280 with v^1 and $\boldsymbol{\tau}^0$ periodic *w.r.t* y_2 , and we have used (11). The system (32) is linear
281 *w.r.t* $\langle \sigma_1^0 \rangle(0, x_2)$ and $\partial_{x_2} u^0(0, x_2)$. Thus, we define $V^{(1)}(\mathbf{y})$ and $V^{(2)}(\mathbf{y})$ such that

$$(33) \quad \left\{ \begin{array}{l} v^1(x_2, \mathbf{y}) = \langle \sigma_1^0 \rangle(0, x_2) V^{(1)}(\mathbf{y}) + \frac{\partial u^0}{\partial x_2}(0, x_2) [A(y_2) + V^{(2)}(\mathbf{y})] + \hat{v}(x_2), \\ \boldsymbol{\tau}^0(x_2, \mathbf{y}) = \langle \sigma_1^0 \rangle(0, x_2) \mathbf{T}^{(1)}(\mathbf{y}) + \frac{\partial u^0}{\partial x_2}(0, x_2) \left[\frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} \mathbf{e}_2 + \mathbf{T}^{(2)}(\mathbf{y}) \right], \end{array} \right.$$

283 with $\mathbf{T}^{(1)}(\mathbf{y}) \equiv \tilde{a}(\mathbf{y}) \nabla V^{(1)}(\mathbf{y})$ and $\mathbf{T}^{(2)}(\mathbf{y}) \equiv \tilde{a}(\mathbf{y}) \nabla V^{(2)}(\mathbf{y})$ (and $A(y_2)$ defined in
284 (23)). Note that the field v^1 in (32) is defined up to a function of x_2 , and it is denoted
285 $\hat{v}(x_2)$ in (33); we shall see that the determination of $\hat{v}(x_2)$ is not needed. It is easy to
286 see that if $(V^{(i)}, \mathbf{T}^{(i)})$ satisfy the elementary problems

$$(34) \quad \left\{ \begin{array}{l} \operatorname{div} \mathbf{T}^{(1)} = 0, \quad \text{with } \mathbf{T}^{(1)}(\mathbf{y}) = \tilde{a}(\mathbf{y}) \nabla V^{(1)}(\mathbf{y}) \\ V^{(1)} \text{ and } \mathbf{T}^{(1)} \cdot \mathbf{n} \text{ continuous,} \\ V^{(1)}, \mathbf{T}^{(1)} \text{ periodic w.r.t. } y_2 \\ \lim_{y_1 \rightarrow -\infty} \nabla V^{(1)}(\mathbf{y}) = \frac{\mathbf{e}_1}{\langle a \rangle}, \quad \lim_{y_1 \rightarrow +\infty} \nabla V^{(1)}(\mathbf{y}) = \mathbf{e}_1, \end{array} \right.$$

288 and

$$(35) \quad \left\{ \begin{array}{l} \operatorname{div} \left[\mathbf{T}^{(2)} + \frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} \mathbf{e}_2 \right] = 0, \quad \text{with } \mathbf{T}^{(2)}(\mathbf{y}) = \tilde{a}(\mathbf{y}) \nabla V^{(2)}(\mathbf{y}), \\ V^{(2)} \text{ and } \left[\mathbf{T}^{(2)} + \frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} \mathbf{e}_2 \right] \cdot \mathbf{n} \text{ continuous,} \\ V^{(2)}, \mathbf{T}^{(2)} \text{ periodic w.r.t. } y_2 \\ \lim_{y_1 \rightarrow -\infty} \nabla V^{(2)}(\mathbf{y}) = \mathbf{0}, \quad \lim_{y_1 \rightarrow +\infty} \nabla V^{(2)}(\mathbf{y}) = -\frac{1/a(y_2) - \langle 1/a \rangle}{\langle 1/a \rangle} \mathbf{e}_2, \end{array} \right.$$

290 then $v^1(x_2, \mathbf{y})$ satisfies (32). The elementary solutions $V^{(1,2)}$ satisfy

$$(36) \quad \left\{ \begin{array}{l} \lim_{y_1 \rightarrow -\infty} \left[V^{(1)} - \frac{y_1}{\langle a \rangle} \right] = -\mathcal{B}, \quad \left\{ \begin{array}{l} \lim_{y_1 \rightarrow -\infty} V^{(2)} = -\mathcal{B}', \\ \lim_{y_1 \rightarrow +\infty} V^{(2)} = -A(y_2). \end{array} \right. \\ \lim_{y_1 \rightarrow +\infty} [V^{(1)} - y_1] = 0, \end{array} \right.$$

292 The above limits are obtained by integrating the limits of $\nabla V^{(i)}$, $i = 1, 2$, thus with
293 unknown constants being *a priori* different at $y_1 \rightarrow \pm\infty$. Next, because $V^{(i)}$ are defined

294 in (34)-(35) up to a constant, we can set the constant equal to zero at $y_1 \rightarrow +\infty$;
 295 for $V^{(1)}$, we denote $-\mathcal{B}$ the constant at $y_1 \rightarrow -\infty$ (it is the first interface parameter).
 296 For $V^{(2)}$, it is denoted $-\mathcal{B}'$; next, $V^{(2)}$ being odd *w.r.t.* y_2 , we have $\mathcal{B}' = 0$. It is
 297 important to stress that the elementary problems, as the unit cell problems in the
 298 classical homogenization, can be solved once and for all, being written in the static
 299 limit. The relations between the elementary solutions $V^{(1,2)}$ and the evanescent fields
 300 in the actual problem (for a given scattering problem) are illustrated in [Appendix A](#).

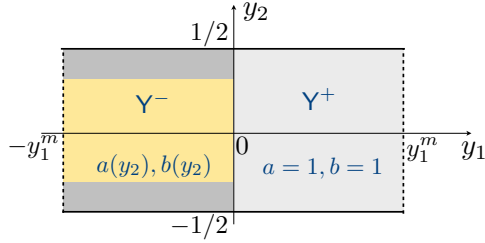


FIGURE 4. The domain $Y = Y^- \cup Y^+$, with $Y^- = (-y_1^m, 0) \times Y$, $Y^+ = (0, +y_1^m) \times Y$. $\bar{a}(\mathbf{y}) = a(y_2)$ and $\bar{b}(\mathbf{y}) = b(y_2)$ in Y^- , and $a = 1 = b$ in Y^+ .

301 **2.3.3. Jump conditions at second-order.** Once the elementary problems are
 302 solved, it is possible to determine the jump conditions.

303 Jump of $\langle u^1 \rangle$ – To get the jump of $\langle u^1 \rangle$, it is sufficient to use the matching conditions
 304 (13a)-(13b) and we want $v^1(x_2, \pm\infty, y_2)$. From (33) along with (36), we have

$$\begin{cases} v^1(x_2, -\infty, y_2) &= \lim_{y_1 \rightarrow -\infty} \left[\left(\frac{y_1}{\langle a \rangle} - \mathcal{B} \right) \langle \sigma_1^0 \rangle(0, x_2) + A(y_2) \frac{\partial u^0}{\partial x_2}(0, x_2) + \hat{v}(x_2) \right], \\ v^1(x_2, +\infty, y_2) &= \lim_{y_1 \rightarrow +\infty} [y_1 \langle \sigma_1^0 \rangle(0, x_2) + \hat{v}(x_2)]. \end{cases}$$

306 Now, we have $\langle \sigma_1^0 \rangle(0, x_2) = \langle a \rangle \partial_{x_1} u^0(0^-, x_2)$ from (20a) and $\langle \sigma_1^0 \rangle(0, x_2) = \partial_{x_1} u^0(0^+, x_2)$
 307 from (16) and (30). Averaging $\llbracket u^1 \rrbracket = u^1(0^+, x_2) - u^1(0^-, x_2, y_2)$ over Y and owing
 308 to $\langle A \rangle = 0$, we get

$$\llbracket \langle u^1 \rangle \rrbracket = \mathcal{B} \langle \sigma_1^0 \rangle(0, x_2).$$

310 Jump of $\langle \sigma_1^1 \rangle$ – The derivation of the jump of σ_1^1 is more tricky, or at least longer. First,
 311 we define $Y \equiv (-y_1^m, y_1^m) \times Y$ (Figure 4) and we shall use the matching conditions
 312 (13c)-(13d) integrated over Y and written in terms of y_1^m

$$\begin{cases} \langle \sigma_1^1 \rangle(0^-, x_2) &= \lim_{y_1^m \rightarrow +\infty} \left[\langle \tau_1^1 \rangle(x_2, -y_1^m) + y_1^m \frac{\partial \langle \sigma_1^0 \rangle}{\partial x_1}(0^-, x_2) \right], \\ \langle \sigma_1^1 \rangle(0^+, x_2) &= \lim_{y_1^m \rightarrow +\infty} \left[\langle \tau_1^1 \rangle(x_2, y_1^m) - y_1^m \frac{\partial \langle \sigma_1^0 \rangle}{\partial x_1}(0^+, x_2) \right]. \end{cases}$$

314 Integrating over Y the Eq. (5a) written at order ε^0 for the inner problem, we get

$$\int_Y d\mathbf{y} \left[\operatorname{div}_{\mathbf{y}} \boldsymbol{\tau}^1(x_2, \mathbf{y}) + \frac{\partial \tau_2^0}{\partial x_2}(x_2, \mathbf{y}) + \tilde{b}(\mathbf{y}) u^0(0, x_2) \right] = 0.$$

316 Two of the three integrals above are easily obtained, namely

$$317 \quad (40) \quad \begin{cases} \int_{\mathcal{Y}} d\mathbf{y} \operatorname{div}_{\mathbf{y}} \boldsymbol{\tau}^1(x_2, \mathbf{y}) = \langle \tau_1^1 \rangle(x_2, y_1^m) - \langle \tau_1^1 \rangle(x_2, -y_1^m), \\ \int_{\mathcal{Y}} d\mathbf{y} \tilde{b}(\mathbf{y}) u^0(0, x_2) = y_1^m [1 + \langle b \rangle] u^0(0, x_2). \end{cases}$$

318 We used, for the first integral, the continuity of $\boldsymbol{\tau}^1 \cdot \mathbf{n}$ and the periodicity of $\boldsymbol{\tau}^1$ *w.r.t.*
319 y_2 . Note that the first integral of (40) corresponds to the first term in $\llbracket \langle \sigma_1^1 \rangle \rrbracket$, from
320 (38). For the second integral, we used (10).

321 Now, let us consider the second integral in (39). First, from (33), we have

$$322 \quad (41) \quad \frac{\partial \tau_2^0}{\partial x_2}(x_2, \mathbf{y}) = \frac{\partial \langle \sigma_1^0 \rangle}{\partial x_2}(0, x_2) T_2^{(1)}(\mathbf{y}) + \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2) \left[\frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} + T_2^{(2)}(\mathbf{y}) \right].$$

323 Next, defining $\mathcal{Y}^- = (-y_1^m, 0) \times Y$, $\mathcal{Y}^+ = (0, +y_1^m) \times Y$, and using (10), we get

$$324 \quad (42) \quad \begin{cases} \int_{\mathcal{Y}^-} d\mathbf{y} \frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2) = y_1^m \langle 1/a \rangle^{-1} \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2), \\ \int_{\mathcal{Y}^+} d\mathbf{y} \frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2) = y_1^m \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2), \end{cases}$$

325 In (42), we want $\partial_{x_1} \langle \sigma_1^0 \rangle$ to appear, in order to absorb the (diverging) terms in y_1^m
326 in the matching condition (38). Do do so, we use (20) for $x_1 < 0$ and (16) for $x_1 > 0$
327 and we get

$$328 \quad (43) \quad \begin{cases} -\frac{\partial \langle \sigma_1^0 \rangle}{\partial x_1}(0^-, x_2) = \langle 1/a \rangle^{-1} \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2) + \langle b \rangle u^0(0, x_2), \\ -\frac{\partial \langle \sigma_1^0 \rangle}{\partial x_1}(0^+, x_2) = \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2) + u^0(0, x_2), \end{cases}$$

329 whence

$$330 \quad (44) \quad \int_{\mathcal{Y}} d\mathbf{y} \left[\frac{\partial^2 u^0}{\partial x_2^2}(0, x_2) \frac{\tilde{a}(\mathbf{y})/a(y_2)}{\langle 1/a \rangle} + \tilde{b}(\mathbf{y}) u^0(0, x_2) \right] = -y_1^m \left[\frac{\partial \langle \sigma_1^0 \rangle}{\partial x_1}(0^+, x_2) + \frac{\partial \langle \sigma_1^0 \rangle}{\partial x_1}(0^-, x_2) \right]. \blacksquare$$

331 It is now sufficient to use (40), (41) and (44) in (39), to get the jump condition

$$332 \quad (45) \quad \llbracket \langle \sigma_1^1 \rangle \rrbracket = -\mathcal{C} \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2), \quad \text{with } \mathcal{C} \equiv \int_{\mathcal{Y}} d\mathbf{y} T_2^{(2)}(\mathbf{y}),$$

333 and we used that $\int_{\mathcal{Y}} d\mathbf{y} T_2^{(1)}(\mathbf{y}) = 0$ since $V^{(1)}$ is symmetric *w.r.t.* y_2 . The constant \mathcal{C}
334 is the second interface parameters entering in the jump conditions.

335 **2.3.4. Jump conditions and final homogenized problem.** The jump condi-
336 tions on $(\bar{u}, \bar{\boldsymbol{\sigma}})$ are deduced from (28), with (29),(30) and (37),(45), and read

$$337 \quad (46) \quad \llbracket \bar{u} \rrbracket = \varepsilon \mathcal{B} \langle \sigma_1^0 \rangle(0, x_2), \quad \llbracket \bar{\boldsymbol{\sigma}}_1 \rrbracket = -\varepsilon \mathcal{C} \frac{\partial^2 u^0}{\partial x_2^2}(0, x_2).$$

338 The above jump conditions define a homogenized problem which can be solved itera-
339 tively : first compute $(u^0, \langle \boldsymbol{\sigma}^0 \rangle)$ satisfying (16), (20) with (29) and (30) (compute also

340 \mathcal{B} and \mathcal{C}) and use the results to get the right hand-side term in (46); then, compute
 341 $(\bar{u}, \bar{\sigma})$ which approximate $(u^\varepsilon, \sigma^\varepsilon)$ up to $O(\varepsilon^2)$. As discussed in [4], it is preferable to
 342 handle a unique problem and this is done by defining the fields $(\tilde{u}, \tilde{\sigma})$ satisfying the
 343 following homogenized problem

$$344 \quad (47) \quad \begin{cases} \operatorname{div} \tilde{\sigma} + \langle b \rangle \tilde{u} = 0, & \tilde{\sigma} = \begin{pmatrix} \langle a \rangle & 0 \\ 0 & \langle 1/a \rangle^{-1} \end{pmatrix} \nabla \tilde{u}, & x_1 < 0 \\ \operatorname{div} \tilde{\sigma} + \tilde{u} = 0, & \tilde{\sigma} = \nabla \tilde{u}, & x_1 > 0 \\ \llbracket \tilde{u} \rrbracket = \frac{\varepsilon \mathcal{B}}{2} [\tilde{\sigma}_1(0^-, x_2) + \tilde{\sigma}_1(0^+, x_2)], \\ \llbracket \tilde{\sigma}_1 \rrbracket = -\frac{\varepsilon \mathcal{C}}{2} \left[\frac{\partial^2 \tilde{u}}{\partial x_2^2}(0^-, x_2) + \frac{\partial^2 \tilde{u}}{\partial x_2^2}(0^+, x_2) \right], \end{cases}$$

345 and it is easy to see from (16), (27) and (46) that $\tilde{u}, \tilde{\sigma}$ admit the expansions $\langle u^0 \rangle +$
 346 $\varepsilon \langle u^1 \rangle, \langle \sigma^0 \rangle + \varepsilon \langle \sigma^1 \rangle$ up to $O(\varepsilon^2)$, thus the same expansion as $(u^\varepsilon, \sigma^\varepsilon)$ up to $O(\varepsilon^2)$.
 347 Finally, coming back to the real space, in $\mathbf{X} = \mathbf{x}/k$ coordinate and with $U(\mathbf{X}) = \tilde{u}(\mathbf{x})$,
 348 $\Sigma(\mathbf{X}) = k \tilde{\sigma}(\mathbf{x})$, (47) take the form

$$349 \quad (48) \quad \begin{cases} \operatorname{div} \Sigma + \langle b \rangle k^2 U = 0, & \Sigma = \begin{pmatrix} \langle a \rangle & 0 \\ 0 & \langle 1/a \rangle^{-1} \end{pmatrix} \nabla U, & X_1 < 0 \\ \operatorname{div} \Sigma + k^2 U = 0, & \Sigma = \nabla U, & X_1 > 0 \\ \llbracket U \rrbracket = \frac{h \mathcal{B}}{2} [\Sigma_1(0^-, X_2) + \Sigma_1(0^+, X_2)], \\ \llbracket \Sigma_1 \rrbracket = -\frac{h \mathcal{C}}{2} \left[\frac{\partial^2 U}{\partial X_2^2}(0^-, X_2) + \frac{\partial^2 U}{\partial X_2^2}(0^+, X_2) \right]. \end{cases}$$

350 The above problem, written for a single interface at $X_1 = 0$, correspond to the system
 351 (3)-(4) when two interfaces at $X_1 = \pm e/2$ are considered.

352 **3. Scattering by an array of rectangular voids.** In this section, we apply
 353 the previous analysis to rectangular voids or cracks, free of stresses (with Neumann
 354 conditions on their boundaries), periodically spaced in a homogeneous matrix being
 355 composed of the same elastic material than the substrate. In electromagnetism, this
 356 corresponds to a (perfect conducting) metallic array in a dielectric or in the air; in
 357 acoustics to an array of sound hard material in a fluid. We consider the scattering of
 358 an incident plane wave U^{inc} arriving from $X_1 < 0$ and hitting the array at oblique
 359 incidence θ (Figure 5), whence

$$360 \quad (49) \quad U^{\text{inc}}(\mathbf{X}) = e^{ik(X_1 + e/2) \cos \theta + ikX_2 \sin \theta}.$$

361 In the actual problem, the solution is sought in the substrate where the Helmholtz
 362 equation apply with Neumann boundary conditions on the boundaries of the voids
 363 occupying the subdomains $\Omega_i, i = 1 \dots N_v$ and $\Omega_v = \cup_i \Omega_i$. The problem is solved in

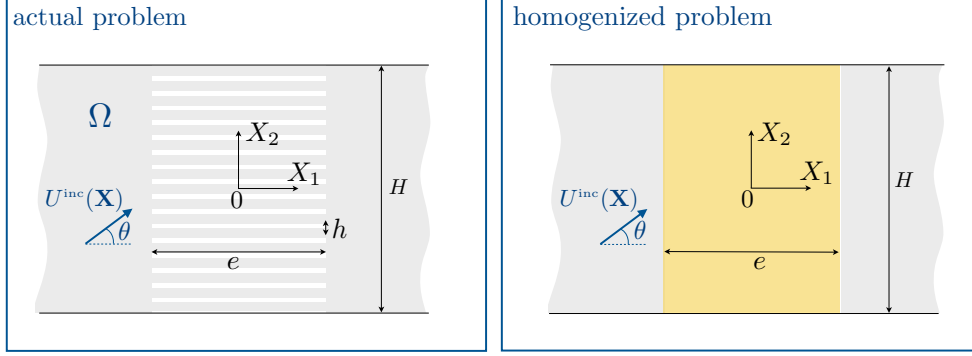


FIGURE 5. *Actual problem of the scattering of a plane wave at oblique incidence θ on an array of rectangular voids; the problem is solved numerically. The homogenized problem involves a slab of same thickness e filled with a homogeneous anisotropic material (the wave equation being (51)); jump conditions (4) apply at $X_1 = \pm e/2$.*

364 $\Omega \setminus \Omega_v$ with $\Omega = \{(X_1, X_2) \in \mathbb{R} \times (-H/2, H/2)\}$ and reads

$$\begin{aligned}
 & \left\{ \begin{array}{l} \Delta U + k^2 U = 0, \\ \nabla U \cdot \mathbf{n} = 0, \end{array} \right. & \begin{array}{l} \text{in } \Omega \setminus \Omega_v, \\ \text{on } \partial\Omega_i, i = 1 \dots N_v, \end{array} \\
 & \lim_{X_1 \rightarrow \pm\infty} \left[\frac{\partial}{\partial X_1} (U - U^{\text{inc}}) \mp ik \cos \theta (U - U^{\text{inc}}) \right] = 0, \\
 & U \left(X_1, \frac{H}{2} \right) = e^{ikH \sin \theta} U \left(X_1, -\frac{H}{2} \right), & X_1 \in \mathbb{R}, \\
 & \frac{\partial U}{\partial X_2} \left(X_1, \frac{H}{2} \right) = e^{ikH \sin \theta} \frac{\partial U}{\partial X_2} \left(X_1, -\frac{H}{2} \right), & X_1 \in \mathbb{R}.
 \end{aligned}
 \tag{50}$$

366 The conditions at $X_1 \rightarrow \pm\infty$ are the radiation conditions required to select an out-
 367 going scattered waves ($U - U^{\text{inc}}$) in the low frequency regime, namely for $k < 2\pi/h$ (if
 368 not the case, the radiation condition should be modified, see [2]). In the case where
 369 $H = nh$, with n an integer (and we shall consider that this is the case), the last condi-
 370 tion is referred to as the condition of pseudo-periodicity or the Floquet condition,
 371 which applies for the incident wave and for the total field [13]. The actual problem is
 372 solved numerically using a multimodal method which reduces to the determination of
 373 a set of scalar coefficients for $|X_1| < e/2$ and for $|X_1| > e/2$ (see subsection S2.2.1).
 374 In the following, the computed solution U^{num} is the reference solution.

375 **3.1. Solutions of the homogenized problems at the first and at the**
 376 **second orders.** We shall see that the homogenized problems at the first two orders
 377 can be solved exactly. Voids or cracks correspond to the limiting case $a = 0 = b$
 378 (leading to Neumann boundary condition at the boundary with any other material).
 379 Next, with $a = 1 = b$ in the substrate, and with φ the filling fraction of the substrate in
 380 the layers, the equivalent medium has bulk parameters $\langle a \rangle = \langle b \rangle = \varphi$ and $\langle 1/a \rangle^{-1} = 0$,
 381 whence the homogenized wave equation (3) becomes

$$382 \tag{51} \quad \text{div} \Sigma + \varphi k^2 U = 0, \quad \Sigma = \begin{pmatrix} \varphi & 0 \\ 0 & 0 \end{pmatrix} \nabla U.$$

383 It follows that the homogenized problems read

$$384 \quad (52) \quad \left\{ \begin{array}{ll} \frac{\partial^2 U}{\partial X_1^2} + k^2 U = 0, & \text{for } |X_1| < \frac{e}{2}, \\ \Delta U + k^2 U = 0, & \text{for } |X_1| > \frac{e}{2}, \\ \text{Jump conditions (4),} & \text{at } X_1 = \pm \frac{e}{2}, \\ \lim_{X_1 \rightarrow \pm\infty} \left[\frac{\partial}{\partial X_1} (U - U^{\text{inc}}) \mp ik \cos \theta (U - U^{\text{inc}}) \right] = 0, & \\ U \left(X_1, \frac{H}{2} \right) = e^{ikH \sin \theta} \left(X_1, -\frac{H}{2} \right), & X_1 \in \mathbb{R}, \\ \frac{\partial U}{\partial X_2} \left(X_1, \frac{H}{2} \right) = e^{ikH \sin \theta} \frac{\partial U}{\partial X_2} \left(X_1, -\frac{H}{2} \right), & X_1 \in \mathbb{R}. \end{array} \right.$$

385 In the following, we refer to the homogenized problems at first and at second orders for
386 the values of $(\mathcal{B}, \mathcal{C})$ entering in the jump conditions (4); at first order, $(\mathcal{B}, \mathcal{C}) = (0, 0)$
387 and at second order,

$$388 \quad (53) \quad \mathcal{B} = -\frac{1}{\pi} \log \sin \left(\frac{\pi \varphi}{2} \right), \quad \mathcal{C} \simeq \frac{\pi}{16} \varphi^2,$$

389 (see [subsection S2.1](#)).

390 The solution of (52) with (49) is of the form

$$391 \quad (54) \quad \left\{ \begin{array}{ll} X_1 < -\frac{e}{2}, & U(\mathbf{X}) = [e^{ik(X_1+e/2) \cos \theta} + R e^{-ik(X_1+e/2) \cos \theta}] e^{ikX_2 \sin \theta}, \\ |X_1| < \frac{e}{2}, & U(\mathbf{X}) = [a e^{ikX_1} + b e^{-ikX_1}] e^{ikX_2 \sin \theta}, \\ X_1 > \frac{e}{2}, & U(\mathbf{X}) = T e^{ik(X_1-e/2) \cos \theta + ikX_2 \sin \theta}, \end{array} \right.$$

392 with (R, T, a, b) given by the jump conditions (4). Indeed, applying (4) to (54), we
393 find, for any (k, θ) values characterizing the incident wave, a set (R, T, a, b) such that
394 U is solution of the homogenized problems. In particular, the scattering coefficients
395 (R, T) read

$$396 \quad (55) \quad \left\{ \begin{array}{l} R = -\frac{z_1^* z_2^* e^{ike} - z_1 z_2 e^{-ike}}{z_1^* z_2^* e^{ike} - z_2^2 e^{-ike}}, \\ T = \frac{|z_1|^2 - |z_2|^2}{z_1^* z_2^* e^{ike} - z_2^2 e^{-ike}}, \end{array} \right.$$

397 (56)

$$398 \quad \left\{ \begin{array}{l} z_1 \equiv \left(1 - \frac{\cos \theta}{\varphi} \right) + ikh \left(\mathcal{B} \cos \theta + \mathcal{C} \frac{\sin^2 \theta}{\varphi} \right) - (kh)^2 \sin^2 \theta \frac{\mathcal{B}\mathcal{C}}{4} \left(1 + \frac{\cos \theta}{\varphi} \right), \\ z_2 \equiv \left(1 + \frac{\cos \theta}{\varphi} \right) - ikh \left(\mathcal{B} \cos \theta - \mathcal{C} \frac{\sin^2 \theta}{\varphi} \right) + (kh)^2 \sin^2 \theta \frac{\mathcal{B}\mathcal{C}}{4} \left(1 + \frac{\cos \theta}{\varphi} \right). \end{array} \right.$$

399 Obviously, for $\mathcal{B} = \mathcal{C} = 0$, the jump conditions (4) simplify to the continuities of U
400 and $\Sigma \cdot \mathbf{n}$ and we recover the usual expressions of the scattering coefficients given by
401 the homogenization at the first order, with $\cos \theta / \varphi$ the effective impedance mismatch
402 between the two media [12]. Finally, the derivation of (a, b) is straightforward and
403 together with (R, T) can be used in (54) to calculate the homogenized wavefield $U(\mathbf{X})$.

404 **3.2. Numerical validation of the homogenized solutions.** We shall inspect
 405 the validity of the homogenized solution up to the first and second orders for an
 406 incident plane wave at normal and at oblique incidences. To begin with, we report the
 407 fields U^{num} calculated numerically and the fields U of the homogenized solutions, (54),
 408 with (55)-(56), for $\varphi = 0.5$ (Figure 6) and $\varphi = 0.9$ (Figure 7); in both cases, $kh = 1$,
 409 $e/h = 10$ and $\theta = \pi/3$. The improvement in the solutions given by the homogenization
 410 at the second order, compared to the ones given by the first order, is visible to the
 411 naked eye. Defining $\Delta U \equiv |U - U^{\text{num}}|/|U^{\text{num}}|$ (for $|X_1| > e/2$ and with $|\cdot|$ the L^2
 412 norm), we get a discrepancy of 10% ($\varphi = 0.5$) and 20% ($\varphi = 0.9$) for the first order
 413 homogenization, and of 0.7%-0.6% for the second order homogenization. It is worth
 noting that a very small error is found even at this relatively large $kh = 1$ value.

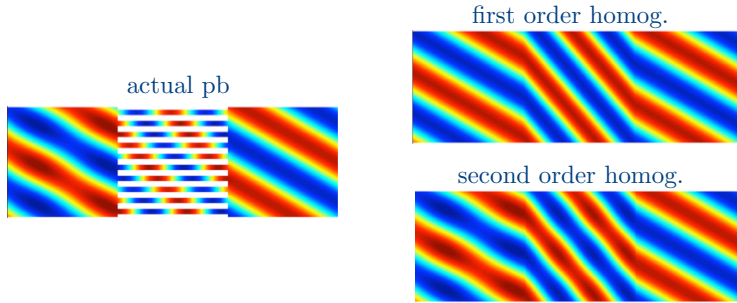


FIGURE 6. Scattering of a plane wave at incidence $\theta = \pi/3$ and $kh = 1$ on an array made of rectangular voids ($e/h = 10$ and $\varphi = 0.5$). The solution U^{num} in the actual problem is calculated numerically; on the right, the fields U given by the homogenization at the first and at the second orders.

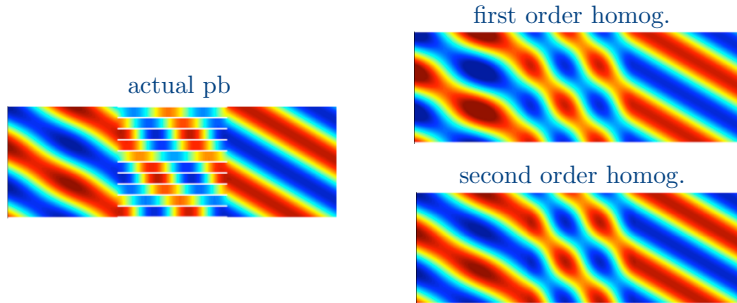


FIGURE 7. Same representation as in Figure 6 with $\varphi = 0.9$.

414

415 **3.2.1. Waves at normal incidence.** We first inspect the case $\theta = 0$, for which
 416 the homogenizations, at first and second orders, impose $[\![\Sigma]\!] \cdot \mathbf{n} = 0$ in (4) (because from
 417 (52), $U(X_1, X_2) = U(X_1, 0)$ does not depend on X_2), thus only the influence of \mathcal{B} in the
 418 jump condition for the displacement is regarded (see also (55) with (56)). We report
 419 in Figure 8 the spectra of the transmission as a function of kh and e/h (with $\varphi = 0.1$
 420 and $\theta = 0$) and in Figure 9 the corresponding errors $\Delta T = |T^{\text{num}} - T|/|T^{\text{num}}|$ (for the
 421 homogenizations at the first and at the second orders). We considered $kh \in [0, 2\pi]$,
 422 $kh = 2\pi$ corresponding to the cut-off frequency above which a second propagating
 423 mode exists in the actual problem.

424 In Figure 9, errors smaller than 1% appear in dark blue and errors greater than

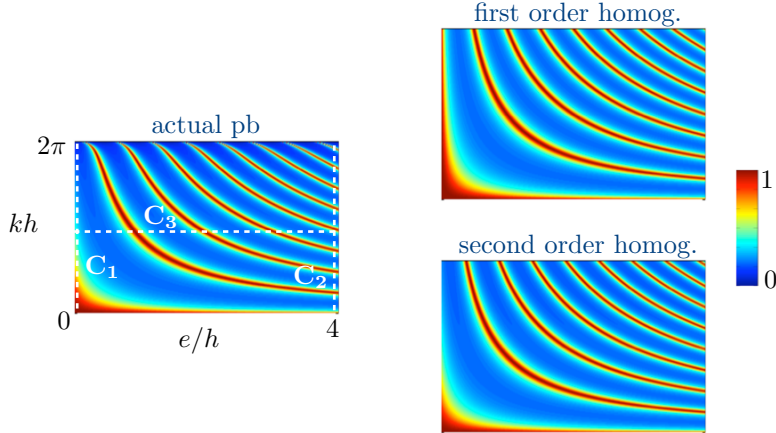


FIGURE 8. Transmission coefficient as a function of e/h and of the frequency kh ; $\varphi = 0.1$ and $\theta = 0$ have been considered. On the left, in the actual problem, $|T^{\text{num}}|$ calculated numerically, and on the right, $|T|$ given by the first and second order homogenizations, (55), with (56).

425 100% in dark red. The range of validity of the homogenized solution is significantly
 426 increased when using the second order homogenization; on the one hand, intermediate
 427 frequencies become accessible (the error is smaller than 4% for $kh < \pi$ in the whole
 428 range of e/h at second order, it is of 50% on average at first order); on the other hand,
 429 the first order homogenization predicts erroneously perfect transmissions for vanishing
 430 thicknesses e/h , while going up to the second order restores the actual scattering
 431 properties of an array of flat voids. This is related to the discussion presented in Ref.
 432 [7] in the context of electromagnetic waves. In this reference, an effective medium
 433 approach at second order is presented assuming the continuities of the displacement
 434 and of the normal stress (instead of our jump conditions); the analysis concludes that
 435 the effective bulk parameter a has to be dependent on the thickness (in this reference,
 a denotes the effective permittivity for electromagnetic waves).

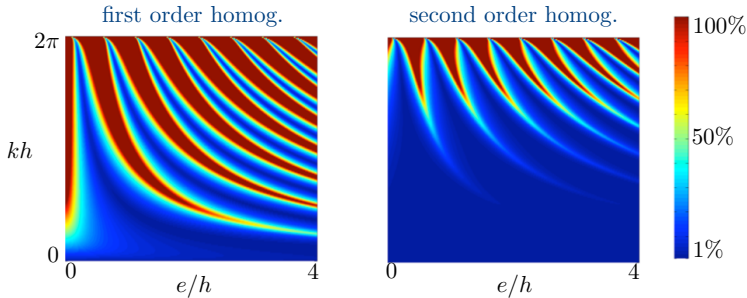


FIGURE 9. Errors ΔT on the transmission coefficient in the homogenization problems (at first and at second orders) as a function of e/h and kh ($\varphi = 0.1$ and $\theta = 0$). Errors below 1% appear in dark blue and errors larger than 100% appear in dark red.

436
 437 More specifically, we inspect (i) the profiles of $|T^{\text{num}}|$ (blue symbols) and its ho-
 438 mogenized counterparts $|T|$ at first order (grey lines) and at second order (black lines)
 439 as a function of kh for $e/h = 0.05$ and $e/h = 4$ (Figure 10). For a small thickness
 440 (C_1 profile from Figure 8), the homogenization at first order largely overestimates
 441 the transmission while including the jump conditions (4) at second order recovers

442 the actual transmission of the array ; for larger array (C_2 profile) the first order ho-
 443 mogenization is valid for small kh and going up to the second order allows us to
 444 increase the range of validity of the homogenized solution. This is because T^{num}
 445 is not periodic *w.r.t.* kh (the kh -distance between two perfect transmissions decreases
 446 as kh increases) ; from (55), this tendency is correctly captured by T at second order,
 447 while T at first order appears to be erroneously periodic, with $2\pi h/e$ period. Finally,
 448 as expected, the errors ΔT vary as kh at the first order and as $(kh)^2$ at the second
 order.

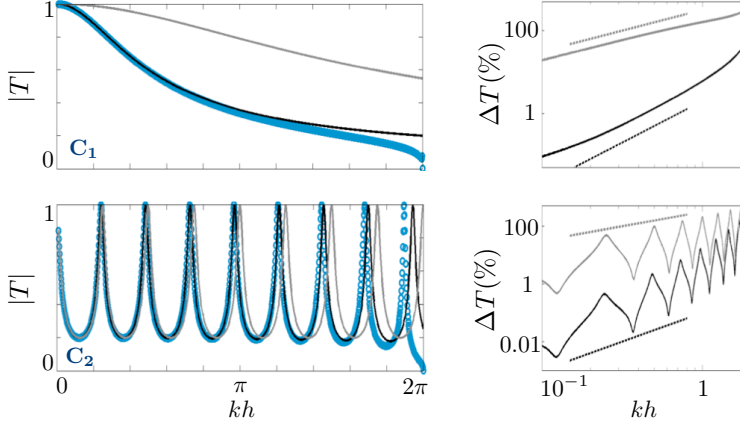


FIGURE 10. Transmission coefficients $|T^{\text{num}}|$ and $|T|$ as a function of kh and corresponding error ΔT of the homogenized predictions. C_1 profile for $e/h = 0.05$ and C_2 for $e/h = 4$ ($|T^{\text{num}}|$: blue symbols and $|T|$: grey lines at first order and black lines at second order). ΔT are shown in %, dotted lines are guidelines with slopes kh (grey) and $(kh)^2$ (black).

449

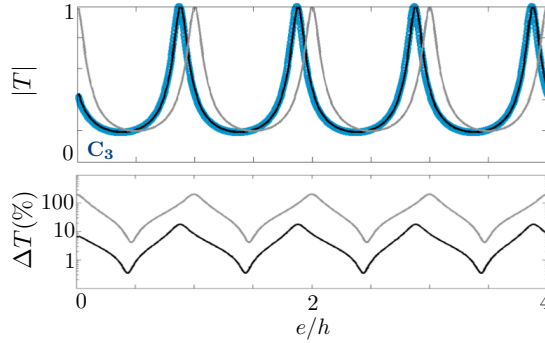


FIGURE 11. Transmission coefficient and errors as a function of e/h for $kh = \pi$ (C_3 profile from Figure 8). Same representation as in Figure 10.

450 (ii) the variations of $|T^{\text{num}}|$ and $|T|$ (and the corresponding errors ΔT) as a func-
 451 tion of e/h for $kh = \pi$ are reported in Figure 11 (C_3 profile from Figure 8). Amusingly,
 452 the large error in the first order homogenization appears to be a direct consequence
 453 of the “initial” error for vanishing e/h ; there, $|T| = 1$ is erroneously found at the
 454 first order, and the periodicity of T *w.r.t.* e/h imposes the same error to occur for any
 455 e/h (the periodicity of T *w.r.t.* e/h is, from (55), $2\pi/kh$, thus equals 2 in the present
 456 case).

457 **3.2.2. The case of oblique incidence.** In the case of oblique incidence ($\theta =$
 458 $\pi/3$ is considered in this section), the difference between the homogenized solutions
 459 at first and second orders involves the two interface parameters (\mathcal{B}, \mathcal{C}). We report
 460 the same sequence of figures as for the normal incidence; with $kh \in [0, 2\pi]$, the
 461 frequency range includes $kh > 2\pi/(1+\sin \theta) \simeq 1.07\pi$ where two modes are propagating
 462 (complete extinction of the first mode is observed at this cut-off frequency, [Figure 12](#)
 463 and [Figure 14](#), corresponding to the Wood anomaly [10]). This range is outside the
 464 range of validity of any homogenization approach since mode coupling is not possible
 at an equivalent flat boundary [10].

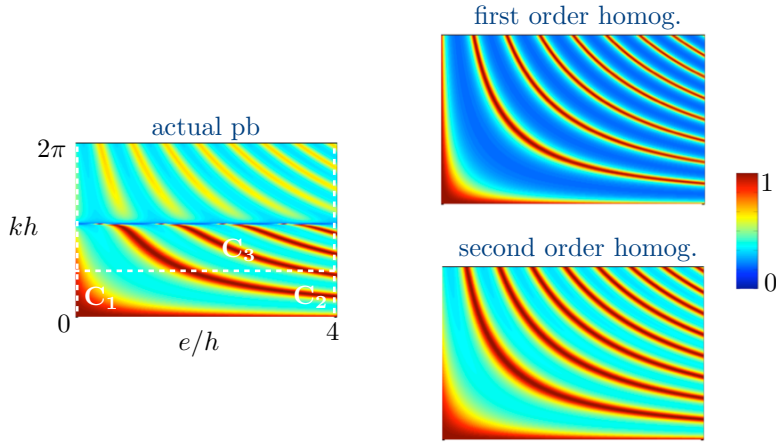


FIGURE 12. Same representation as [Figure 8](#) for $\theta = \pi/3$.

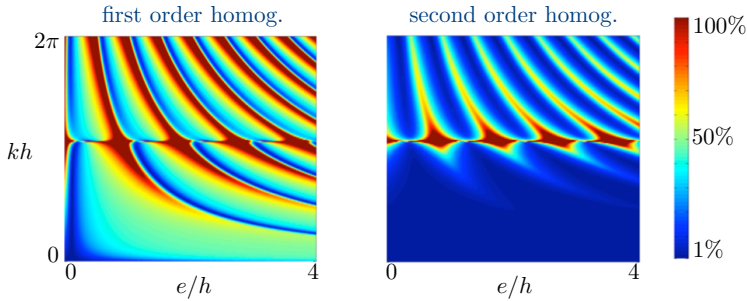
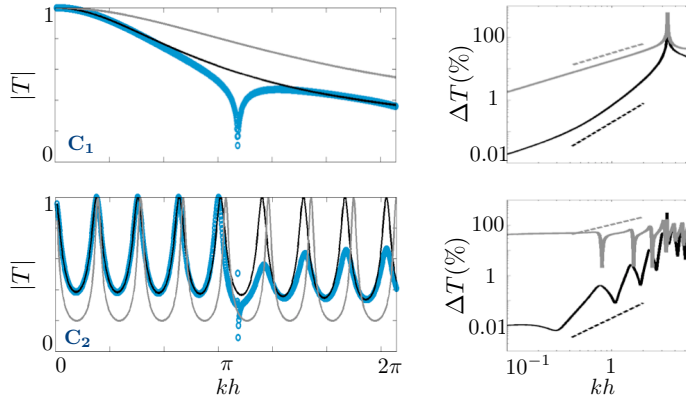
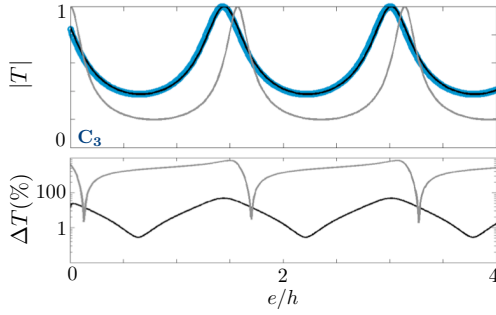


FIGURE 13. Same representation as [Figure 9](#) for $\theta = \pi/3$.

465 Inspecting [Figure 12](#) to [Figure 15](#), we recover in general the same tendencies
 466 as those observed at normal incidence. On average, for $kh < \pi/2$, the error in the
 467 transmission coefficient is smaller than 1% in the whole range of e/h at second order, it
 468 is of 40% on average at first order. Also, the first order homogenization underestimates
 469 the scattering properties of the structure when e/h goes to zero (C_1 profile in [Figure 14](#)
 470 and [Figure 15](#)). Reversely for larger e/h , and this is more surprising, it overestimates
 471 the scattering properties (with $|T|$ significantly smaller than $|T^{\text{num}}|$) even for small
 472 kh value (from [Figure 12](#) and the C_2 profile in [Figure 14](#)). Thus, in general, the
 473 improvement in the second order homogenized solution is even more significant at an
 474 oblique incidence.
 475

FIGURE 14. Same representation as Figure 10 for $\theta = \pi/3$.FIGURE 15. Transmission coefficient and errors as a function of e/h for $kh = 0.6\pi$ (C_3 profile from Figure 12). Same representation as in Figure 10.

476 **4. Concluding remarks.** The homogenization that we have presented explicitly
 477 accounts for the finite size e/h of stratified structures. At first and at second
 478 orders, this makes effective bulk parameters to appear which are simply averages of
 479 the bulk parameters in each layer and these effective bulk parameters enter in the
 480 homogenized wave equation. Note the simplicity happening in the case of stratified
 481 media : (i) the bulk parameters are found without solving cell problems, and this is
 482 well known, (ii) the same effective wave equation is found at first and at second orders,
 483 and this is less known. Note also that this simplicity would be lost in the case of
 484 periodic media with a more complex unit cell. Finally, the most significant improvement
 485 in the presented approach is the derivation of jump conditions involving effective
 486 interface parameters when accounting for the finite thickness of the structure. More
 487 usually, the continuity of the displacement and of the normal stress are assumed, and
 488 this is what we recover at first order. Going up to second order allows us to establish
 489 jump conditions for these fields and the improvement in the homogenized result has
 490 been exemplified.

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496 10-IDEX-0001-02 PSL*.

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499

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532 **Annexe A. The case of vanishing slab thicknesses.** The validity of the
 533 homogenization of stratified media with finite size has been exemplified in this paper
 534 for varying e/h . In fact, the case of vanishing thicknesses has to be inspected more
 535 carefully. Indeed, we end with jump conditions reflecting the behavior of the evanes-
 536 cent field at each boundary of the equivalent slab, *and these boundary layers have*
 537 *been assumed to be independent.* In fact, for very small thicknesses, the two boundary
 538 layers may interact. In this case, the bulk problem is meaningless and the elementary
 539 problems have to include the whole structure; doing so, jump conditions across an
 540 equivalent interface are found (and the bulk behavior is disregarded), see [9, 11]. We
 541 obtained in this case

$$542 \quad (57) \quad \begin{cases} R^{\text{int}} = -\frac{1}{2} \left[\frac{Z_1^*}{Z_1} + \frac{Z_2^*}{Z_2} \right], \\ T^{\text{int}} = \frac{1}{2} \left[\frac{Z_1^*}{Z_1} - \frac{Z_2^*}{Z_2} \right], \end{cases}$$

543

$$544 \quad (58) \quad \begin{cases} Z_1 = 1 - ikh \cos \theta \left(\mathcal{B} + \frac{e}{2\varphi} \right), \\ Z_2 = -i \cos \theta - kh \left(\frac{e\varphi}{2h} + \mathcal{C} \sin^2 \theta \right), \end{cases}$$

545 with $(\mathcal{B}, \mathcal{C})$ in (53). Here, we illustrate the limitation of the present homogenization
 in the light of the size of the boundary layers in the actual problem.

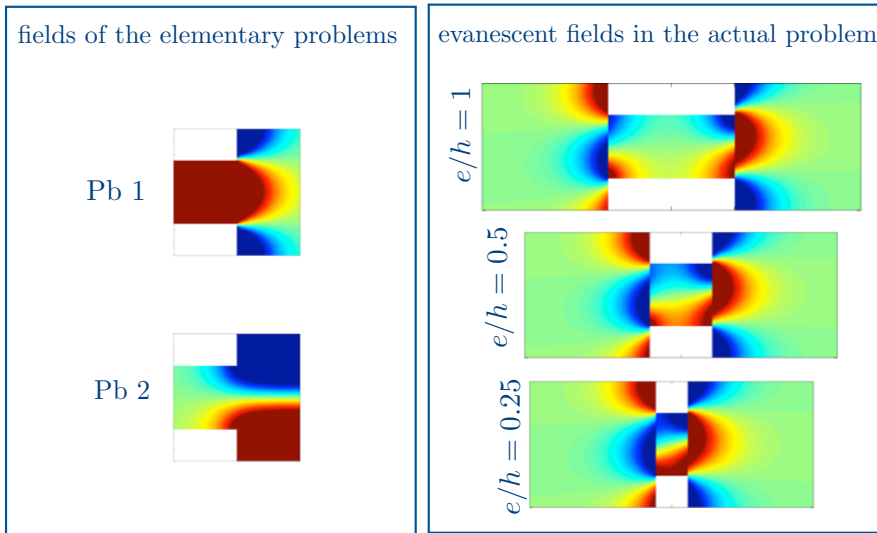


FIGURE 16. *Boundary layers in the static elementary problems and evanescent fields in the actual problems for $\varphi = 0.5$. In the actual problem, we considered $kh = 1$ and $\theta = \pi/4$.*

546

547 In Figure 16, we reported (i) the elementary solutions $V^{(1,2)}$ of (S9) and (S17) for
 548 $\varphi = 0.5$ (for $V^{(1)}$, the external load is (y_1) and it has been removed to exhibit the
 549 resulting boundary layer), (ii) the evanescent fields in the actual problem for $kh = 1$
 550 and varying $e/h = 1, 0.5$ and 0.25 (the total wavefields are continuous but the evanes-
 551 cent fields are not). Qualitatively, for $e/h = 1$, it is visible that the evanescent

552 fields in the actual problem resemble (by parts) to the fields in the elementary pro-
 553 blems. This is quite natural if one remembers that the evanescent field in the actual
 554 problem can be decomposed in modes with y_1 dependance being of the form $e^{\pm ik_n y_1}$,
 555 and $k_n = \sqrt{k^2 - (n\pi/h)^2} \sim i(n\pi/h)$ for $y_1 > 0$, $k_n = \sqrt{k^2 - (n\pi/h\varphi)^2} \simeq i(n\pi/h\varphi)$
 556 for $y_1 < 0$, thus involving at the dominant order the same y_1 dependences as in the
 557 static problems (see subsection S2.2.1). Decreasing e result in the interaction of the
 558 evanescent fields within the array, or in other words the whole array is concerned by
 559 the boundary layer effects.

560 Quantitatively, Figure 17 shows T^{num} and T (at second order) and the resulting
 561 error ΔT as a function of e/h in logscale up to $e/h = 10^{-2}$ (and $\varphi = 0.1, 0.5$ and
 562 0.9). It is visible that the error significantly increases for $e/h < 1$, and the increase is
 563 more significant for larger φ ; to estimate more carefully the critical thickness below
 564 which the present homogenization is not valid anymore (or say less accurate), one
 565 should consider the influence of φ (φ being a measure of the size of boundary layer,
 566 to be compared to e/h the array thickness in \mathbf{y} -coordinates). We report in dotted
 567 lines the transmission coefficient T^{int} given by the interface homogenization (57)-(58)
 568 (from [9]). As expected, this homogenization which accounts for the boundary layers
 569 in the whole array, is more accurate for vanishing thickness.

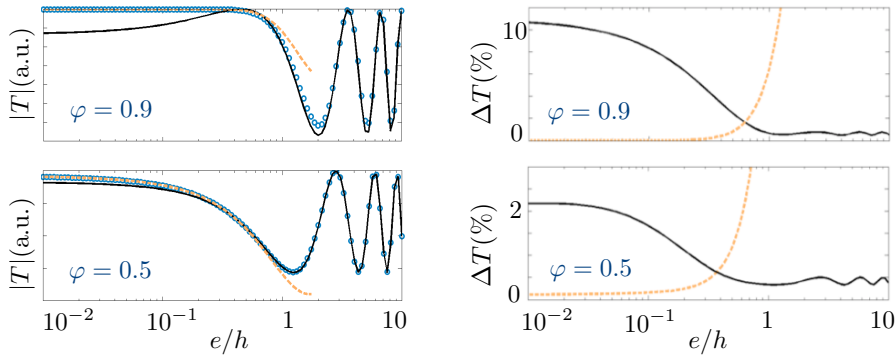


FIGURE 17. Transmission coefficient $|T^{\text{num}}|$ (blue symbols) and $|T|$ at second order (black lines) as a function of e/h for $\varphi = 0.9$ and 0.5 , and corresponding errors ΔT . The errors increase significantly for roughly $e/h < 1$. Dotted orange lines show the transmission coefficient $|T^{\text{int}}|$ obtained using interface homogenization (57)-(58) (from [9]).